OBJECTIVES:

To expose the students to the operation of D.C. machines and transformers and give them experimental skill.

LIST OF EXPERIMENTS:

1. Open circuit and load characteristics of DC shunt generator- critical resistance and critical speed.
2. Load characteristics of DC compound generator with differential and cumulative connections.
3. Load test on DC shunt and compound motor.
4. Load test on DC series motor.
5. Swinburne’s test and speed control of DC shunt motor.
7. Load test on single-phase transformer and three phase transformers.
8. Open circuit and short circuit tests on single phase transformer.
9. Polarity Test and Sumpner’s test on single phase transformers.
10. Separation of no-load losses in single phase transformer.
11. Study of starters and 3-phase transformers connections

TOTAL: 45 PERIODS

OUTCOMES:

- Ability to model and analyze electrical apparatus and their application to power system
EE6411 – Electrical Machines-1 Laboratory
IV Semester - Electrical and Electronics Engineering
Duration: 2014-2015(EVEN SEMESTER)
INDEX

1. Open circuit and load characteristics of separately and self excited DC shunt generators.
2. Load characteristics of DC compound generator with differential and cumulative connection.
3. Load characteristics of DC shunt and compound motor.
4. Load characteristics of DC series motor.
5. Swinburne’s test and speed control of DC shunt motor.
7. Load test on single-phase transformer and three phase transformer connections.
8. Open circuit and short circuit tests on single phase transformer.
9. Polarity Test and Sumpner’s test on single phase transformers.
10. Separation of no-load losses in single phase transformer.
11. Study of starters and 3-phase transformers connections
### CYCLE-I

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</table>
EXP.NO.

DATE:

OPEN CIRCUIT AND LOAD CHARACTERISTICS OF SEPAREATELY EXCITED D.C SHUNT GENERATOR

AIM:
To obtain open circuit and load characteristics of separately excited d.c shunt generator.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Ammeter</td>
<td>(0-1)A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>Voltmeter</td>
<td>(0-300)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Rheostats</td>
<td>400Ω, 0.8A</td>
<td>Wire</td>
<td>2</td>
</tr>
</tbody>
</table>

PRECAUTION
- All the switches are kept open initially.
- The motor field rheostat is kept at minimum resistance position.
- The generator field rheostat is kept at maximum resistance position.

PROCEDURE
OPEN CIRCUIT CHARACTERISTICS:-
- The connections are made as per the circuit diagram.
- After checking minimum position of motor field rheostat, maximum position of generator field rheostat, the supply side DPST switch is closed and starting resistance is gradually removed.
- The motor is started using three point starter.
- By varying the field rheostat of the motor, the speed of the motor is adjusted to the rated speed of the generator.
- By varying the generator field rheostat, voltmeter and ammeter readings are taken.
- After bringing the generator rheostat to maximum position, field rheostat of motor to minimum position, the DPST switch is closed.
CIRCUIT DIAGRAM

TABULAR COLUMN:

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Field current, ( I_f ) Amperes</th>
<th>Generated EMF, ( E_g ) volts</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td></td>
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<td>2.</td>
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<td>8.</td>
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<td>9.</td>
<td></td>
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<tr>
<td>10.</td>
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<td></td>
</tr>
</tbody>
</table>
MODEL GRAPH:-

OPEN CIRCUIT CHARACTERISTICS:-

\[ E_g (V) \]

\[ R_V \]

\[ I_f (A) \]

MODEL CALCULATION:-

Armature current, \( I_a = I_L = I_f \)
Generated EMF, \( E_g = (V + I_a R_a) \)

LOAD TEST:

- Keeping the generator side DPST open, the field rheostat in the generator side is adjusted for the rated voltage of the generator which is seen in the voltmeter.
- Now the DPST switch is closed and the resistive load is put up on the generator step by step. The terminal voltage, armature and load current values are noted down for each step from the respective meters.
- Note that while taking each set of readings, the field current is maintained constant as that for rated voltage [because due to heating, shunt field resistance is increased]
**TABULAR COLUMN:**

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Voltage, $V_L$ (Volts)</th>
<th>Current, $I_L$ (Amperes)</th>
<th>Armature Current, $I_a$ (Amperes)</th>
<th>Generated EMF, $E_g$ (Volts)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
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</tbody>
</table>

**MODEL GRAPH:**

**LOAD TEST:**

![Graph showing EMF, $E_g$ vs Voltage, $V$, and Current, $I_a$ vs $I_L$.]

**MODEL CALCULATION:**

Armature current, $I_a = I_L = I_f$

Generated EMF, $E_g = (V + I_a R_a)$

**RESULT:**

Thus the open circuit and load characteristics of separately excited D.C. shunt generator were drawn.
EXP.NO.

DATE:

OPEN CIRCUIT AND LOAD CHARACTERISTICS
OF SELF EXCITED D.C SHUNT GENERATOR

AIM:

To obtain the open circuit and load characteristics of a self-excited DC shunt generator and hence deduce the critical field resistance and critical speed.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0 - 2A)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0 - 10A)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0 - 300V)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400 /1.1 A, 800 /0.8 A</td>
<td>Wire wound</td>
<td>1 each</td>
</tr>
</tbody>
</table>

PRECAUTION

- All the switches are kept open initially.
- The motor field rheostat is kept at minimum resistance position.
- The generator field rheostat is kept at maximum resistance position.

PROCEDURE

OPEN CIRCUIT CHARACTERISTICS:-

- The connections are made as per the circuit diagram.
- After checking minimum position of motor field rheostat, maximum position of generator held rheostat. The DPST switch is closed and starting resistance is gradually removed.
- The motor is started using three point starter.
- By varying the field rheostat of the motor, the speed of the motor is adjusted to the rated speed of the generator.
• By varying the generator field rheostat, voltmeter and ammeter readings are taken in steps upto 120% of rated voltage.
• After bringing the generator rheostat to maximum position, field rheostat of motor to minimum position, the DPST switch is closed.
• Draw $R_e$ line, such that it is tangent to the initial portion of O.C.C. at rated speed and passes through origin.
CIRCUIT DIAGRAM
TABULAR COLUMN FOR OPEN CIRCUIT CHARACTERISTICS

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Field current, $I_f$ Amperes</th>
<th>Generated EMF, $E_g$ volts</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
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<td>2.</td>
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<td>3.</td>
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</table>

MEASUREMENT OF $R_{sh}$ FOR GENERATOR:

![Circuit Diagram 1]

MEASUREMENT OF $R_a$ FOR GENERATOR:

![Circuit Diagram 2]
### Measurement of $R_A$:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>$V$ (Volts)</th>
<th>$I$ (Amps)</th>
<th>$R_{sh}$ (Ohms)</th>
</tr>
</thead>
<tbody>
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</tbody>
</table>

### Measurement of $R_{sh}$:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>$V$ (Volts)</th>
<th>$I$ (Amps)</th>
<th>$R_a$ (Ohms)</th>
</tr>
</thead>
<tbody>
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</tbody>
</table>

**Model Graph:**

Model Calculation:

O.C.C

$$E_0 \propto N$$

So, for different speeds, O.C.C. can be deduced from the O.C.C at rated speed.

$$\frac{N_1}{N_2} = \frac{E_1}{E_2}$$

Critical field resistance, $R_c = \text{the slope of } R_c \ 	ext{line} = \frac{OA}{OC}$

Critical speed, $N_c = \frac{BC}{AC} \times N_{R\ (N)}$

Where $N_R$ is the Rated speed.

**Model Graph:**

![Model Graph Image](image-url)
LOAD TEST:

- The connections are made as per the circuit diagram.
- The motor is started using three point starter.
- Run the MG set at rated speed
- Excite the Generator to its rated voltage after closing the SPSTS, and observe the readings on no load.
- Close the DPSTS on load side, vary the load for convenient steps of load current and observe the meter readings.
- Note that on each loading the speed should be rated speed.
- Load the Generator upto its rated capacity.

TABULAR COLOUMN FOR LOAD CHARACTERISTICS

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Terminal Voltage (V) Volts</th>
<th>Load Current (I_L) Amps</th>
<th>I_f (Amps)</th>
<th>I_a (Amps)</th>
<th>E_g = V + I_aR_a (Volts)</th>
</tr>
</thead>
<tbody>
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</tbody>
</table>

MODEL CALCULATION:

Load test:

For self excitation I_a = I_L + I_f

So, induced emf on load, E_g = V + I_aR_a
MODEL GRAPHS:

![Graph of \( E_g \) vs \( V \), \( E_g \) vs \( I_d \), and \( V \) vs \( I_L \)](image)

RESULT:

Thus the open circuit and load characteristics of self excited D.C. shunt generator were drawn.
LOAD TEST ON D.C. COMPOUND GENERATOR WITH DIFFERENTIAL AND CUMULATIVE CONNECTION

AIM
To conduct the load test on the given D. C. compound generator in the following modes.

1. Cumulative
2. Differential

APPARATUS REQUIRED:-

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0-2)A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0-15)A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0-300)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400 /1.1A, 1000 /1A</td>
<td>Wire wound</td>
<td>1 each</td>
</tr>
</tbody>
</table>

PRECAUTION

- All the switches should be kept open.
- The field rheostat of the motor should be kept at minimum resistance position.
- The field rheostat of the generator should be kept at maximum resistance position.

PROCEDURE

- The connections are made as per the circuit diagram.
- The DPST switch is closed.
- The motor is started using four point starter.
- The field rheostat of the motor is adjusted to bring the motor speed to the rated speed of the generator.
- The generator field rheostat is adjusted till the voltmeter reads the rated voltage of the generator.
- DPST switch on the generator side is closed.
- The load is increased in steps.
- At each step of loading all the meter readings are noted.
- The above procedure is repeated till the ammeter reads the rated current.
- Switch off the load gradually and make the motor and generator rheostat resistance position as instructed in the precaution.
- Turn off the supply
- Interchange the terminal connection of the generator series field coil and repeat the procedure right from the first step.
CIRCUIT DIAGRAM

CUMULATIVE SHUNT

DIFFERENTIAL SHUNT
**TABULAR COLUMN**

**CUMULATIVE**

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>$I_L$ (A)</th>
<th>$V_L$ (V)</th>
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**DIFFERENTIAL**

<table>
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<tr>
<th>Sl. No.</th>
<th>$I_L$ (A)</th>
<th>$V_L$ (V)</th>
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</table>

**MODEL GRAPHS:**

![Graph](cumulative_vs_differential.png)
RESULT

Thus the performance characteristics of the DC compound generator were drawn.
LOAD CHARACTERISTICS OF D.C SHUNT MOTOR

AIM:

1. To determine the efficiency of D.C shunt motor.

2. To obtain the performance characteristics of shunt motor.

APPARATUS REQUIRED

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0 - 2A)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0 - 10A)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0 - 300V)</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400 /1.1A,</td>
<td>Wire wound</td>
<td>1 each</td>
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<td></td>
<td></td>
<td>600 /1.2A</td>
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PRECAUTIONS:

At the time of switching on and switching off the supply,

- The field rheostat should be at the minimum resistance position.
- There should not be any load on the motor.
CIRCUIT DIAGRAM FOR BRAKE TEST ON D.C. SHUNT MOTOR:

220V DC Supply

2 Point Switch

(0-300)V MC

(0-5)A MC

400Ω 1.1A

3 Point Starter

Brake Drum

F1

F2

A1

A2
**TABULAR COLUMN**

Radius of brake drum, \( r = \) _______ mts.

<table>
<thead>
<tr>
<th>S.N o.</th>
<th>V (Volts)</th>
<th>I (Amps)</th>
<th>Spring Balance (Kg)</th>
<th>Speed N (rpm)</th>
<th>Torque T (Nm)</th>
<th>Output Power ( P_o ) (Watts)</th>
<th>Input Power ( P_i ) (Watts)</th>
<th>Efficiency ( \eta ) %</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>( F_1 )</td>
<td>( F_2 )</td>
<td>( F_1 - F_2 )</td>
<td></td>
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</tbody>
</table>

**MODEL GRAPHS:**

![Graph 1](image1.png)

![Graph 2](image2.png)
RESULT:

Thus the performance characteristics of the DC shunt motor were drawn.
EXP:

DATE:

LOAD TEST ON D.C. COMPOUND MOTOR

AIM

To perform the load test on the given DC compound motor and draw the performance characteristics.

APPARATUS REQUIRED:-

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0 - 20) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0 - 2) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0 - 300) V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400 Ω, 1.1 A</td>
<td>-</td>
<td>1</td>
</tr>
</tbody>
</table>

PROCEDURE

- The connections are given as per the circuit diagram.
- The DPST switch is closed.
- The motor is started using the four point starter.
- The speed of the motor is adjusted to the rated value by varying the field rheostat.
- The no load readings are noted.
- The load on the brake drum increased in steps.
- At each step of loading the meter readings are noted.
- The procedure is repeated till the ammeter reads the rated current.

PRECAUTION

- All the switches are kept open initially.
- The field rheostat should be kept at minimum resistance position.
- There should not be any load when start and stop the motor.
- While starting the motor, the starter handle is moved slowly from OFF to ON position.
- While running on load, the brake drum should be cooled by pouring water inside the brake drum.
CIRCUIT DIAGRAM:
FORMULA USED:

Circumference of brake drum = $2 \times \pi \times R$ in meter

R – Radius of the brake drum

Torque, $T = \left( S_1 - S_2 \right) \times 9.81 \times R$ in Nm

Input power, $P_i = V_L \times I_L$ in Watts

Output power, $P_0 = \left( 2 \times \pi \times N \times T \right) / 60$ in Watts

% Efficiency, $\eta = \left( P_0 / P_i \right) \times 100$

TABULAR COLOMN

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Voltage, $V_L$ (V)</th>
<th>Current, $I_L$ (A)</th>
<th>Spring balance</th>
<th>Speed Rpm</th>
<th>$S_1$ $S_2$ kg</th>
<th>Torque N-m</th>
<th>Input $P_i$ watts</th>
<th>Output $P_m$ watts</th>
<th>Efficiency In %</th>
</tr>
</thead>
<tbody>
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MODEL GRAPHS:
RESULT:

Thus the performance characteristics of the DC compound motor were drawn.
LOAD TEST ON D.C. SERIES MOTOR

AIM:
- To determine the efficiency of D.C series motor.
- To obtain the performance characteristics of series motor.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0-15)A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Voltmeter</td>
<td>(0-300)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Rheostat</td>
<td>400 /1.14A,</td>
<td>Wire wound</td>
<td>1</td>
</tr>
</tbody>
</table>

PRECAUTION:
The motor should be started with some initial load.

PROCEDURE:
- Connections are given as per circuit diagram.
- Before starting the motor some initial load is applied to the motor by using the brake drum with spring balance.
- Using two-point starter the motor is started to run.
- The meter readings are started at its initial condition.
- Gradually load the machine up to rated current and corresponding meter readings were noted.
- After the observation of all the readings the load is released gradually up to the initial load condition.
FORMULAE USED:

Circumference of the brake drum = _____ cms

Radius of the brake drum, \( r = _____ \) m

Torque applied on the shaft of the rotor, \( T = (F1 - F2) \times r \times 9.81 \) Nm

Output power, \( P_o = 2\pi x \frac{N \times T}{60} \) Watts

Input power \( P_i = V \times I_L \) Watts

Efficiency, \( = \frac{P_o}{P_i} \)
CIRCUIT DIAGRAM FOR BRAKE TEST ON D.C. SERIES MOTOR:

2 Point Starter

Fuse

(0-20A)MC

(0-300V)MC

Brake Drum

220 V D.C.

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Observation:

Radius of brake drum, \( r = \boxed{\text{mts}} \).

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Voltage ( V_L ) (Volts)</th>
<th>Current ( I_L ) (Amps)</th>
<th>Spring Balance (Kg)</th>
<th>Speed ( N ) (rpm)</th>
<th>Torque ( T ) (Nm)</th>
<th>Output Power ( P_o ) (Watts)</th>
<th>Input Power ( P_i ) (Watts)</th>
<th>Efficiency ( \eta )%</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>( F_1 )</td>
<td>( F_2 )</td>
<td>( F_1 - F_2 )</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Model Graphs:

RESULT:

Thus the performance characteristics of the DC series motor were drawn.
EXP.NO:
DATE

SWINBURNE’S TEST

AIM:
To predetermined the efficiency of the D.C. machine when it act as
(i) Motor
(ii) Generator

APPARATUS REQUIRED:-

<table>
<thead>
<tr>
<th>Sl.No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0 -5) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0 - 2) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0 - 300)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400, 1.1 A</td>
<td>Wire wound</td>
<td>1</td>
</tr>
<tr>
<td>5.</td>
<td>Tachometer</td>
<td></td>
<td>Digital</td>
<td>1</td>
</tr>
</tbody>
</table>

PRECAUTION:

1. The field rheostat should be kept at minimum resistance position.
2. There should be no load at the time of starting the experiment.

PROCEDURE:

1. The connections are made as per the circuit diagram.
2. The DPST switch is closed.
3. The motor is started with the help of three point starter.
4. The field rheostat of the motor is adjusted to bring the motor speed to the rated value.
5. The no load current, voltage and shunt field current are noted.

FORMULA USED:

\[ W_c = VI_a - (I_O - I_f)^2 R_a \]

\[ R_a \] – Resistance of armature

31
For Motor

- Armature Current \( I_a = I_L - I_f \)
- Armature copper loss \( W_{cu} = I_a^2 R_a \)
- Total loss \( W_t = W_c + W_{cu} \)
- Input power \( P_I = V I_L \)
- Output Power \( P_o = P_I - W_t \)
- Efficiency \( \eta = \frac{\text{Output Power}}{\text{Input power}} \times 100 \)

For Generator

- Armature Current \( I_a = I_L + I_f \)
- Armature copper loss \( W_{cu} = I_a^2 R_a \)
- Total loss \( W_t = W_c + W_{cu} \)
- Output power \( P_o = V I_L \)
- Input Power \( P_I = P_o + W_t \)
- Efficiency \( \eta = \frac{\text{Output Power}}{\text{Input power}} \times 100 \)

**TABULAR COLUMN**

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Voltage, V (volts)</th>
<th>Field current, ( I_f ) (A)</th>
<th>No load current, ( I_0 ) (A)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
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<td></td>
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<td></td>
<td></td>
</tr>
</tbody>
</table>

For generator

<table>
<thead>
<tr>
<th>Line Current, ( I_L ) (A)</th>
<th>Field current ( I_f ) (A)</th>
<th>( I_a = I_L + I_f ) (A)</th>
<th>( W_{cu} = I_a^2 R_a )</th>
<th>Constant Loss</th>
<th>Total Loss (watts)</th>
<th>Input Power (watts)</th>
<th>Output Power (watts)</th>
<th>Efficiency ( % \eta )</th>
</tr>
</thead>
</table>
For motor

<table>
<thead>
<tr>
<th>Line Current, $I_L$ (A)</th>
<th>Field current $I_f$ (A)</th>
<th>$I_a = I_L - I_f$ (A)</th>
<th>$W_{cu} = I_a^2 R_a$</th>
<th>Constant Loss</th>
<th>Total Loss (watts)</th>
<th>Input Power (watts)</th>
<th>Output Power (watts)</th>
<th>Efficiency % $\eta$</th>
</tr>
</thead>
</table>

Measurement of $R_a$:

<table>
<thead>
<tr>
<th>Voltage (v)</th>
<th>Current (A)</th>
<th>Armature resistance $R_a$ (ohms)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Model Graph

RESULT:
Thus the efficiency of the DC machine has been predetermined and characteristics were drawn.
EXP.NO: 
DATE: 

SPEED CONTROL OF D.C. SHUNT MOTOR

AIM
To draw the speed characteristics of DC shunt motor by
(1) Armature control method
(2) Field control method

APPARATUS REQUIRED:-

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Ammeter</td>
<td>(0 - 5) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Ammeter</td>
<td>(0 - 2) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Voltmeter</td>
<td>(0 - 300)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Rheostat</td>
<td>400, 1.1 A</td>
<td>Wire wound</td>
<td>1</td>
</tr>
<tr>
<td>5.</td>
<td>Tachometer</td>
<td>Digital</td>
<td></td>
<td>1</td>
</tr>
</tbody>
</table>

PRECAUTION:

1. All the switches are kept open initially.
2. The field rheostat should be kept at minimum resistance position.
3. The armature rheostat should be kept at maximum resistance position.

PROCEDURE:

ARMATURE CONTROL METHOD:-

1. The connections are given as per the circuit diagram.
2. The DPST switch is closed.
3. The field current is varied in steps by varying the field rheostat.
4. In each step of field current the armature voltage is varied in steps by varying the armature rheostat.
5. In each step of armature rheostat variation the meter readings (Voltmeter & Tachometer) are noted.
CIRCUIT DIAGRAM:

[Diagram of a circuit with 3 Point Starter, 220V DC Supply, DPST Switch, and other components labeled with currents and specifications.]
FIELD CONTROL METHOD:-

1. The connections are given as per the circuit diagram.
2. The DPST switch is closed.
3. The armature voltage is varied in steps by varying the armature rheostat.
4. In each step of armature voltage the field current in steps by varying the field rheostat.
5. In each step of field rheostat the meter readings (Ammeter & tachometer) are noted.

TABULAR COLUMN:

ARMATURE VOLTAGE CONTROL:

<table>
<thead>
<tr>
<th>S.No</th>
<th>( I_{F1} = ) A</th>
<th>( I_{F2} = ) A</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Voltage V</td>
<td>Speed N rpm</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

FIELD CONTROL:

<table>
<thead>
<tr>
<th>S.No</th>
<th>Voltage ( V_1 = ) V</th>
<th>Voltage ( V_2 = ) V</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Field current ( I_F ) A</td>
<td>Field current ( I_F ) A</td>
</tr>
<tr>
<td></td>
<td>Speed N rpm</td>
<td>Speed N rpm</td>
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</tbody>
</table>

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RESULT:

Thus the speed characteristics of the DC shunt motor were drawn.
EXP NO:
DATE:

HOPKINSON’S TEST

AIM:

To conduct Hopkinson’s test on a pair of identical DC machines to pre-determine the efficiency of the machine as generator and as motor.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Ammeter</td>
<td>(0-1)A (0-10)A</td>
<td>MC</td>
<td>1</td>
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<tr>
<td></td>
<td></td>
<td></td>
<td>MC</td>
<td>2</td>
</tr>
<tr>
<td>2</td>
<td>Voltmeter</td>
<td>(0-300)V (0-600)V</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Rheostats</td>
<td></td>
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</tbody>
</table>

PRECAUTIONS:

1. The field rheostat of the motor should be in the minimum position at the time of starting and stopping the machine.
2. The field rheostat of the generator should be in the maximum position at the time of starting and stopping the machine.
3. SPST switch should be kept open at the time of starting and stopping the machine.

PROCEDURE:

1. Connections are made as per the circuit diagram.
2. After checking the minimum position of field rheostat of motor, maximum position of field rheostat of generator, opening of SPST switch, DPST switch is closed and starting resistance is gradually removed.
3. The motor is brought to its rated speed by adjusting the field rheostat of the motor.
4. The voltmeter \( V_1 \) is made to read zero by adjusting field rheostat of generator and SPST switch is closed.
5. By adjusting field rheostats of motor and generator, various Ammeter readings, voltmeter readings are noted.
6. The rheostats and SPST switch are brought to their original positions and DPST switch is opened.
CIRCUIT DIAGRAM
TABULAR COLUMN:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Supply Voltage $V_S$ (V)</th>
<th>$I_S$ (A)</th>
<th>$I_{FM}$ (A)</th>
<th>$V_A$ (A)</th>
<th>$I_{FG}$ (A)</th>
<th>$I_{LG}$ (A)</th>
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</thead>
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</table>

AS MOTOR:

<table>
<thead>
<tr>
<th>$I_{LG}$ (A)</th>
<th>Armature Cu Loss W (Watts)</th>
<th>Field Loss (Watts)</th>
<th>Stray loss / Machine (Watts)</th>
<th>Total Losses $W_t$ (Watts)</th>
<th>O/P Power (W)</th>
<th>I/p Power (W)</th>
<th>% $\eta$</th>
</tr>
</thead>
<tbody>
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</tbody>
</table>

www.Vidyarthiplus.com
AS GENERATOR:

<table>
<thead>
<tr>
<th>$I_{LG}$ (A)</th>
<th>Armature Cu Loss W (Watts)</th>
<th>Field Loss (Watts)</th>
<th>Stray loss / Machine (Watts)</th>
<th>Total Losses $W_t$ (Watts)</th>
<th>O/P Power (W)</th>
<th>I/p Power (W)</th>
<th>% $\eta$</th>
</tr>
</thead>
<tbody>
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</tbody>
</table>

FORMULAE:

Input Power = $VI_1$ watts

Motor armature cu loss = $(I_1 + I_2)^2 Ra$ watts

Generator armature cu loss = $I_2^2 Ra$ watts

Total Stray losses $W$ = $V I_1 - (I_1+I_2)^2 Ra + I_2^2 Ra$ watts.

Stray loss per machine = $W/2$ watts.

AS MOTOR:

Input Power = Armature input + Shunt field input

= $(I_1 + I_2) V + I_3 V = (I_1+I_2+I_3) V$

Total Losses = Armature Cu loss + Field loss + stray loss

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\[ = (I_1 + I_2)^2 Ra + VI_3 + W/2 \text{ watts} \]

Input power – Total Losses

Efficiency \( \eta \% \) = \----------------------------- x 100% 

Input Power

**AS GENERATOR:**

Output Power = \( VI_2 \) watts

Total Losses = Armature Cu loss + Field Loss + Stray loss

= \( I_2^2 Ra + VI_4 + W/2 \) watts

Output power

Efficiency \( \eta \% \) = \----------------------------- x 100% 

Output Power + Total Losses

**MODEL GRAPH:**

RESULT:

Thus Hopkinson’s test is conducted on a pair of identical DC machines the efficiency of the machine as generator and as motor are pre-determined.
LOAD TEST ON SINGLE PHASE TRANSFORMER

AIM:

To determine the efficiency
To find the variation of secondary terminal voltage with respect to the load current.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Item</th>
<th>Type</th>
<th>Range</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Auto Transformer</td>
<td>230/(0-270) V, 1φ</td>
<td>-</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>Wattmeter</td>
<td>300 V, 5A</td>
<td>UPF</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>150 V, 5 A</td>
<td>UPF</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Ammeter</td>
<td>(0-10) A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(0-5) A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>4</td>
<td>Voltmeter</td>
<td>(0-300) V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(0-150) V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>5</td>
<td>Connecting Wires</td>
<td>2.5sq.mm</td>
<td>Copper</td>
<td>Few</td>
</tr>
<tr>
<td>6</td>
<td>Load</td>
<td>(5 KW,230V)</td>
<td>-</td>
<td>1</td>
</tr>
</tbody>
</table>

PRECAUTION:

1. The Variac should be kept in minimum position while switching on and switching off the supply side DPSTS.

2. At the time of switching on the supply there should not be any load connected.
RANGE FIXING:

Rated primary current, \( I_1 = \frac{Rated \ capacity \ in \ VA}{Primary \ voltage \ V_1} \)

Rated secondary current, \( I_2 = \frac{Rated \ capacity \ in \ VA}{Secondary \ voltage \ V_2} \)

The load used is resistive in nature.

\[ \therefore \text{The range of } A_p, V_p, W_p \text{ are } \ldots \ldots \ldots \text{A, } \ldots \ldots \ldots \text{V, } \ldots \ldots \ldots \text{W respectively.} \]

\[ \text{The range of } A_s, V_s, W_s \text{ are } \ldots \ldots \ldots \text{A, } \ldots \ldots \ldots \text{V, } \ldots \ldots \ldots \text{W respectively.} \]

PROCEDURE:

1. Excite the transformer to its rated voltage on no load.
2. Observe the meter readings at no load.
3. Gradually load the transformer and note the meter readings for each loading.
4. Load the transformer to its rated capacity i.e. till it draws rated current from the supply.

Note that applied voltage to the primary side should be kept at its rated voltage on loading.

FORMULA USED:

Output power \( = W_s \)

Input Power \( = W_p \)

\[ \% \ \eta = \frac{W_s}{W_p} \times 100 \]

\[ \% \ \text{Regulation} = \frac{V_{s0} - V_s}{V_{s0}} \times 100 \] (where \( V_{s0} \) – no load secondary rated terminal voltage)
CIRCUIT DIAGRAM:

VRL - Variable Resistive Load
### TABULAR COLUMN:

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>( V_P ) Volts</th>
<th>( I_P ) Amps</th>
<th>( W_P ) (Watts)</th>
<th>( V_S ) Volts</th>
<th>( I_S ) Amps</th>
<th>( W_S ) (Watts)</th>
<th>% Efficiency</th>
<th>% Regulation</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

### MODEL GRAPHS:

- **Efficiency Graph:** %\( \eta \) vs. Input Power (\( P_0 \))
- **Voltage Regulation Graph:** %\( \text{regulation} \) vs. Secondary Voltage (\( V_S \))

### RESULT:

Thus the efficiency and regulation of a three-phase transformer were calculated.
LOAD TEST ON A THREE PHASE TRANSFORMER

AIM:

Determination of Regulation & Efficiency of three-phase transformer by direct loading.

APPARATUS REQUIRED:-

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Name of the apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Voltmeter</td>
<td>0-600 V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>2.</td>
<td>Voltmeter</td>
<td>0-300 V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>3.</td>
<td>Ammeter</td>
<td>0-10A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>4.</td>
<td>Ammeter</td>
<td>0-20A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>5.</td>
<td>Wattmeter</td>
<td>600V,5/10A,UPF</td>
<td></td>
<td>1</td>
</tr>
<tr>
<td>6.</td>
<td>Resistive load</td>
<td>3ph 415V,5kw</td>
<td></td>
<td>1</td>
</tr>
</tbody>
</table>

PRECAUTIONS:

All the switches should be kept open.
The auto transformer should be kept at minimum potential position.

PROCEDURE:

1) Connect the circuit as shown in figure.
2) Keep load on transformer at off position.
3) Keeping dimmer stat at zero position, switch on 3-Phase supply.
4) Now increase dimmer stat voltage for 440 V.
5) Note down the no-load readings.
6) Then increase the load in steps till rated current of the transformer & note down corresponding readings.
7) Calculate efficiency & regulation for each reading.
CIRCUIT DIAGRAM:

3PHASE 440 V, SUPPLY

WATTMETER 10 A, 600 V, DOUBLE ELEMENT TYPE

440/220 V, 5 KVA 3 PHASE TRANSFORMER

3 PHASE 5 KW RESISTIVE LOAD

20 A, 300 V WATTMETER DOUBLE ELEMENT TYPE
MODEL CALCULATION:

- Input power = $W_1 + W_2$ Watts
- Output power = $\sqrt{3} V_2 I_2$ Watts
- % Efficiency = \frac{\text{output}}{\text{Input}} \times 100$
- % Regulation = \frac{V_{NL} - V_L}{V_L}$

TABULAR COLUMN

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>V1 Volts</th>
<th>I1 Amperes</th>
<th>W1 Watts</th>
<th>V2 Volts</th>
<th>I2 Amperes</th>
<th>W2 Watts</th>
<th>Efficiency</th>
<th>Regulation</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
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<td></td>
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<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

RESULT:

Thus the efficiency and regulation of a three phase transformer were calculated.
EXP. NO:

DATE:

OPEN CIRCUIT AND SHORT CIRCUIT TESTS ON SINGLE-PHASE TRANSFORMER

AIM:

1. To obtain the equivalent circuit of transformer.
2. To predetermine the efficiency and regulation of transformer.
3. To predetermine the maximum efficiency of transformer

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Item</th>
<th>Type</th>
<th>Range</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Ammeter</td>
<td>MI</td>
<td>(0-2A)</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>(0-5A)</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>Voltmeter</td>
<td>MI</td>
<td>(0-150V)</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Wattmeter</td>
<td>LPF</td>
<td>(150V,2A)</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>UPF</td>
<td>(150V,5A)</td>
<td>1</td>
</tr>
</tbody>
</table>
| 4     | Connecting wires | Copper | Few

PRECAUTION:

1. Variac must be kept in minimum position while switching on and switching off the supply.
2. LPF wattmeter for O.C. test and UPF wattmeter for S.C. circuit test should be used.

RANGE FIXING:

O.C. Test:

Full load primary current \( I_L = \frac{\text{Full load capacity in VA}}{\text{Primary voltage} V_1} \)
Full load secondary current \[ I_2 = \frac{\text{Full load capacity in VA}}{\text{Secondary voltage} V_2} \]

Let both O.C. and S.C. test be conducted on primary side.

On O.C. test the current drawn by the transformer is about 5 – 10% of Full load Primary current. ∴ Ammeter range is (0 - ) A

The rated primary voltage will be applied. ∴ Voltmeter range (0 - ) V

Observation:

O.C. Test:  

S.C. Test:

\[
\begin{array}{|c|c|c|} 
\hline
V_0 & I_0 & W_0 \text{ (Watts)} \\
\hline
\text{Observed} & \text{Actual} & \\
\hline
\end{array}
\]

\[
\begin{array}{|c|c|c|} 
\hline
V_{sc} & I_{sc} \text{ (Amps)} & W_{sc} \text{ (Watts)} \\
\hline
\text{Observed} & \text{Actual} & \\
\hline
\end{array}
\]

M.F. =  

M.F. =
EQUIVALENT CIRCUIT OF THE TRANSFORMER REFERRED TO PRIMARY SIDE:

CIRCUIT DIAGRAM FOR O.C. & S.C. TESTS ON SINGLE PHASE TRANSFORMER:

O.C. TEST:

![O.C. Test Circuit Diagram](image)

S.C. TEST:

![S.C. Test Circuit Diagram](image)
MODEL GRAPHS:

WATTMETER:

The current rating and voltage rating of Wattmeter are to be nearer to the value calculated above.

On O.C. condition the reactive power drawn is more and the active power drawn is less.

So power factor on no-load will be very low.

∴ LPF wattmeter can be used.

The range of wattmeter is \( V, \ A, \ LPF \).

S.C. TEST:

The voltage applied to the transformer primary to circulate rated full load current is about 5 to 10% of rated primary voltage.

∴ The voltmeter range is (0 - \( V \))

Ammeter range is (0 - \( A \))

The active power drawn by the transformer on S.C. condition is more and reactive power drawn is less.∴ UPF wattmeter can be used.

Range of wattmeter is \( V, \ A, \ UPF \).
PROCEDURE:

1. With the help of Variac, apply rated voltage to the transformer in O.C. test and circulate rated current in S.C. test. Note down the corresponding meter readings.

MODEL CALCULATION:

1) EQUIVALENT CIRCUIT:

Power factor on no load  \[ \cos \phi_0 = \frac{W_0}{V_0 I_0} \]

Working component of no load current, \( I_w = I_0 \cos \phi_0 \)

Magnetising component of no load current, \( I_\mu = I_0 \sin \phi_0 \)

Resistance to account iron losses, \( R_0 = \frac{V_0}{I_w} \)

Reactance to account magnetization of the core, \( X_0 = \frac{V_0}{I_\mu} \)

Equivalent resistance of the transformer referred to primary, \( R_{01} = \frac{W_{sc}}{I_{sc}} \)

(assuming S.C. test is conducted on primary side)
### Predetermination of Efficiency:

<table>
<thead>
<tr>
<th>S. No.</th>
<th>% of load</th>
<th>Copper loss T.L. = $W_c = X^2 W_{sc}$ (Watts)</th>
<th>Cos$\phi$ = 1</th>
<th>Cos$\phi$ = 0.8</th>
<th>Cos$\phi$ = 0.6</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>$W_i + W_c$ (Watts)</td>
<td>$P_o$ (Watts)</td>
<td>$P_o$ (Watts)</td>
<td>$P_o$ (Watts)</td>
</tr>
<tr>
<td>1</td>
<td>0</td>
<td></td>
<td>$P_i$ (Watts)</td>
<td>$P_i$ (Watts)</td>
<td>$P_i$ (Watts)</td>
</tr>
<tr>
<td>2</td>
<td>20</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
<tr>
<td>3</td>
<td>40</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
<tr>
<td>4</td>
<td>60</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
<tr>
<td>5</td>
<td>80</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
<tr>
<td>6</td>
<td>100</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
<tr>
<td>7</td>
<td>120</td>
<td></td>
<td>$\eta$</td>
<td>$\eta$</td>
<td>$\eta$</td>
</tr>
</tbody>
</table>
PREDETERMINATION OF FULL LOAD REGULATION:

<table>
<thead>
<tr>
<th>S.No.</th>
<th>CosΦ</th>
<th>SinΦ</th>
<th>% Regulation</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0</td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>0.2</td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>0.4</td>
<td></td>
<td></td>
</tr>
<tr>
<td>4</td>
<td>0.6</td>
<td></td>
<td></td>
</tr>
<tr>
<td>5</td>
<td>0.8</td>
<td></td>
<td></td>
</tr>
<tr>
<td>6</td>
<td>1.0</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Equivalent impedance of the transformer referred to primary, \( Z_{01} = \frac{V_{sc}}{I_{sc}} \)

Equivalent leakage reactance of the transformer referred to primary, \( X_{01} = \sqrt{Z_{01}^2 - R_{01}^2} \)

Voltage transformation ratio, \( K = \frac{V_2}{V_1} \)

Equivalent resistance of the transformer referred to secondary, \( R_{02} = K^2 R_{01} \)

Equivalent leakage reactance of the transformer referred to secondary, \( X_{02} = K^2 X_{01} \).

\( I_2' \) – Secondary rated current referred to Primary side

\( V_2' \) – Secondary rated voltage referred to Primary side
II) PREDETERMINATION OF EFFICIENCY:

Let the load be x% of FL kVA and cosφ - load power factor

Power output, \( P_0 = x \times (FL \text{ kVA}) \times cosφ \times 1000 \)

Copper Losses, \( W_c = x^2 W_{sc} \)

Total Losses, \( W = W_i + W_c \) (where \( W_i \)is approx. equal to \( W_0 \))

Power input \( P_i = P_0 + W \)

Efficiency, \( \eta = \frac{P_0}{P_i} \)

III) PREDETERMINATION OF FULL LOAD REGULATION:

\[
\text{% Regulation} = \left( \frac{I_2 R_{02} \cos\phi + I_2 X_{02} \sin\phi}{V_2} \right) \times 100
\]

Where \( I_2 \)- Full load secondary current.

\( V_2 \)- rated secondary voltage

\( \cos\phi \)- Load power factor

+ve sign for lagging power factor load

-ve sign for leading power factor load

IV) MAXIMUM EFFICIENCY – PREDETERMINATION:

For maximum \( \eta \), copper loss = Iron loss

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i.e. $I_2^2 R_{02} = W_i$

Load current corresponding to maximum efficiency $I_2 = \sqrt{\frac{W}{R_{02}}}$

Then, maximum $\eta$ can be determined for any load power factor as below.

Cos $\phi$-- load power factor (assume)

Power output, $P_o = V_2 I_2 \cos \phi$

Total losses, $W = 2 W_i$

Power output, $P_o = P_i + W$

Maximum efficiency $\eta_{\text{max}} = \frac{P_o}{P_i} \times 100$

RESULT:

Thus the efficiency and regulation of the single phase transformer was predetermined and equivalent circuit was drawn.
EXP.NO: POLARITY TEST ON SINGLE PHASE TRANSFORMER

DATE:

AIM:
To determine the polarity of a single phase transformer

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S. No.</th>
<th>Name of the Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Auto Transformer</td>
<td>230/(0-270) V</td>
<td>-</td>
<td>2</td>
</tr>
<tr>
<td>2</td>
<td>Voltmeter</td>
<td>(0-600)V</td>
<td>MI</td>
<td>3</td>
</tr>
<tr>
<td>3</td>
<td>Connecting Wires</td>
<td>2.5sq.mm</td>
<td>Copper</td>
<td>Few</td>
</tr>
</tbody>
</table>

PRECAUTION:

1. Auto transformer must be kept in minimum position while switching on and switching off the supply.
2. Transformer should be operated under rated values.

PROCEDURE:

1. Connect the circuit as shown circuit diagram.
2. Switch on the single phase AC supply.
3. Record the voltages $V_1$, $V_2$, and $V_3$. In case $V_3 < V_1$ polarity is subtractive. terminals A1 and a2. In case $V_3 > V_1$ polarity is additive.
CIRCUIT DIAGRAM:

TABULAR COLUMN:

Subtractive polarity:

<table>
<thead>
<tr>
<th>S.No</th>
<th>V_1</th>
<th>V_2</th>
<th>V_3 = V_2 - V_1</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Additive polarity:

<table>
<thead>
<tr>
<th>S.No</th>
<th>V_1</th>
<th>V_2</th>
<th>V_3 = V_2 + V_1</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

RESULT:

Thus the Polarity of a given single phase Transformer is determined by conducting a polarity test.
EXP.NO:
DATE:

SUMPNER'S TESTON TRANSFORMERS

AIM:
To predetermine the efficiency and regulation of a given single phase Transformer by conducting back-to-back test.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S. No.</th>
<th>Name of the Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Auto Transformer</td>
<td>230/(0-270) V</td>
<td>-</td>
<td>2</td>
</tr>
<tr>
<td>2</td>
<td>Wattmeter</td>
<td>150 V, 2 A</td>
<td>LPF</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>150 V, 5 A</td>
<td>UPF</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Ammeter</td>
<td>(0-2) A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(0-5) A</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>4</td>
<td>Voltmeter</td>
<td>(0-75) V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td></td>
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<td>(0-150) V</td>
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<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(0 -600) V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>5</td>
<td>Connecting Wires</td>
<td>2.5 sq.mm</td>
<td>Copper</td>
<td>Few</td>
</tr>
</tbody>
</table>

PRECAUTIONS:
1. Auto Transformer should be kept in zero position, before switching on the ac supply.
2. Transformer should be operated under rated values.

FORMULA USED:

www.Vidyarthiplus.com
Core loss = $W_0$

Copper Loss = full load cu loss $X (1/x)^2$

Total loss = Core loss + Cu loss

Output = $V_2 I_2 \cos \phi$

Input = output + total loss

% Efficiency = output/input * 100

**POWER FACTOR ON NO LOAD:**

$\cos \Phi = (W_o / V_o I_o)$

Working component $I_W = I_o \cos \Phi$

Magnetizing component $I = I_o \sin \Phi$

Resistance $R_o = V_o / I_w$ in

**FOR SHORT CIRCUIT TEST:**

Equivalent resistance $R_{01} = W_{sc} / I_{sc}^2$ in

Equivalent impedance $Z_{01} = V_{sc} / I_{sc}$ in

Equivalent leakage reactance $X_{01} = \sqrt{(Z_{01}^2 - R_{01}^2)}$ in

Voltage ratio = $V_2 / V_1$

$R_{02} = K^2 \times R_{01}$

$X_{02} = K^2 \times X_{01}$

**PERCENTAGE OF REGULATION**

Lagging PF = $(I_2 R_{02} \cos \Phi + I_2 X_{02} \sin \Phi) / V_2$

Leading PF = $(I_2 R_{02} \cos \Phi - I_2 X_{02} \sin \Phi) / V_2$

**PROCEDURE:**

1. Connections are made as shown in the circuit diagram.
2. Rated voltage of 110V is adjusted to get in voltmeter by adjusting the variac of the Auto Transformer which would be in zero before switching on the supply at the primary side.
3. The readings of voltmeter, ammeter and wattmeter are noted on the primary side.
4. A voltmeter is connected across the secondary and with the secondary supply off i.e switch S is kept open. The voltmeter reading is noted.
5. If the reading of voltmeter reads higher voltage, the terminals of any one of secondary coil is interchanged in order that voltmeter reads zero.
6. The secondary is now switched on and SPST switch is closed with variac of auto transformer is zero.

7. After switching on the secondary the variac of transformer (Auto) is adjusted so that full load rated secondary current flows.

8. Then the readings of wattmeter, Ammeter and voltmeter are noted.

9. The Percentage Efficiency and percentage regulation are calculated and equivalent circuit is drawn.

CIRCUIT DIAGRAM:
TABULAR COLUMN:

<table>
<thead>
<tr>
<th>$V_O$ (V)</th>
<th>$I_O$ (A)</th>
<th>$W_O$ (watts)</th>
<th>$V_{Sc}$ (V)</th>
<th>$I_{Sc}$ (A)</th>
<th>$W_{Sc}$ (watts)</th>
</tr>
</thead>
<tbody>
<tr>
<td>OBSERVED</td>
<td>ACTUAL</td>
<td></td>
<td>OBSERVED</td>
<td>ACTUAL</td>
<td></td>
</tr>
</tbody>
</table>

To find Efficiency

<table>
<thead>
<tr>
<th>Load</th>
<th>Core loss $W_o$ (Watts)</th>
<th>Cu loss $W_c$(Watts)</th>
<th>Total loss $W_T$(watts)</th>
<th>Output power $W_o$(watts)</th>
<th>Input power $W_i$(watts)</th>
<th>$% \eta$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>UPF 0.8</td>
<td>UPF 0.8</td>
<td>UPF 0.8</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

To find Regulation

<table>
<thead>
<tr>
<th>Load</th>
<th>Cos$\phi$</th>
<th>Sin$\phi$</th>
<th>$I_2$Re$\phi$</th>
<th>$I_2$Xe$\phi$</th>
<th>$%$ Regulation</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>LAG</td>
<td>LEAD</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

RESULT:

Thus the efficiency and regulation of a given single phase Transformer is carried out by conducting back-to-back test.
EXP NO:
DATE:

SEPARATION OF NO LOAD LOSSES IN A SINGLE PHASE TRANSFORMER

AIM:
To separate no load losses of a transformer in to eddy current loss and hysteresis loss.

APPARATUS REQUIRED:

<table>
<thead>
<tr>
<th>S. No.</th>
<th>Name of the Apparatus</th>
<th>Range</th>
<th>Type</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Rheostat</td>
<td>400 Ω, 1.1 A</td>
<td>Wire Wound</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>Wattmeter</td>
<td>300 V, 5 A</td>
<td>LPF</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Ammeter</td>
<td>(0-2) A</td>
<td>MC</td>
<td>1</td>
</tr>
<tr>
<td>4</td>
<td>Voltmeter</td>
<td>(0-300) V</td>
<td>MI</td>
<td>1</td>
</tr>
<tr>
<td>5</td>
<td>Connecting Wires</td>
<td>2.5 sq.mm</td>
<td>Copper</td>
<td>Few</td>
</tr>
</tbody>
</table>

PRECAUTIONS:
1. The motor field rheostat should be kept at minimum resistance position.
2. The alternator field rheostat should be kept at maximum resistance position.

PROCEDURE:
1. Connections are given as per the circuit diagram.
2. Supply is given by closing the DPST switch.
3. The DC motor is started by using the 3 point starter and brought to rated speed by adjusting its field rheostat.
4. By varying the alternator filed rheostat gradually the rated primary voltage is applied to the transformer.
5. The frequency is varied by varying the motor field rheostat and the readings of frequency are noted and the speed is also measured by using the tachometer.
6. The above procedure is repeated for different frequencies and the readings are tabulated.
7. The motor is switched off by opening the DPST switch after bringing all the rheostats to the initial position.
CIRCUIT DIAGRAM:

![Circuit Diagram Image]

- 3 point starter
- 220V DC Supply
- 250Ω, 5.5A
- 400Ω, 1.1A
- 300V, 5A, LPF
- Fuse

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<table>
<thead>
<tr>
<th>S.No.</th>
<th>Speed N (rpm)</th>
<th>Frequency f (Hz)</th>
<th>Voltage V (Volts)</th>
<th>Wattmeter reading Watts</th>
<th>Iron loss Wi (Watts)</th>
<th>W_i/f Joules</th>
</tr>
</thead>
<tbody>
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</table>
FORMULAE USED:
1. Frequency, \( f = \frac{(P \times N_s)}{120} \) in Hz
   \( P = \) No. of Poles & \( N_s = \) Synchronous speed in rpm.
2. Hysteresis Loss \( W_h = A \times f \) in Watts \( A = \) Constant (obtained from graph)
3. Eddy Current Loss \( W_e = B \times f^2 \) in Watts \( B = \) Constant (slope of the tangent drawn to the curve)
4. Iron Loss \( W_i = W_h + W_e \) in Watts
   \( \frac{W_i}{f} = A + (B \times f) \)
   Here the Constant A is distance from the origin to the point where the line cuts the Y-axis in the graph between \( \frac{W_i}{f} \) and frequency f.
   The Constant B is \( \frac{(W_i/f)}{f} \)

MODEL GRAPH:

RESULT:
Thus separation of eddy current and hysteresis loss from the iron loss on a single-phase transformer is conducted.
STUDY OF STARTERS AND THREE PHASE CONNECTIONA OF A TRANSFORMER

AIM:
To Study about the starters and three phase connection of a transformer.

EQUIPMENT REQUIRED:

<table>
<thead>
<tr>
<th>Sl No.</th>
<th>Name of the apparatus</th>
<th>Quantity</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Two Point starter</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>Three Point starter</td>
<td>1</td>
</tr>
<tr>
<td>3</td>
<td>Four Point starter</td>
<td>1</td>
</tr>
<tr>
<td>4</td>
<td>DOL Starter</td>
<td>1</td>
</tr>
<tr>
<td>5</td>
<td>Auto transformer Starter</td>
<td>1</td>
</tr>
<tr>
<td>6</td>
<td>Star-Delta Starter</td>
<td>1</td>
</tr>
<tr>
<td>7</td>
<td>Rotor Resistance Starter</td>
<td>1</td>
</tr>
</tbody>
</table>

THEORY:
The value of the armature current in a D.C shunt motor is given by

\[ I_a = \frac{(V - E_b)}{R_a} \]

Where \( V \) = applied voltage.

\( R_a = \) armature resistance.

\( E_b = \) Back e.m.f.

In practice the value of the armature resistance is of the order of 1 ohms and at the instant of starting the value of the back e.m.f is zero volts. Therefore under starting conditions the value of the armature current is very high. This high inrush current at the time of starting may damage the motor. To protect the motor from such dangerous current the D.C motors are always started using starters.
The types of D.C motor starters are

i) Two point starters

ii) Three point starters

iii) Four point starters.

The functions of the starters are

i) It protects the from dangerous high speed.

ii) It protects the motor from overloads.

**i) TWO POINT STARTERS: (refer fig 1)**

It is used for starting D.C. series motors which has the problem of over speeding due to the loss of load from its shaft. Here for starting the motor the control arm is moved in clock-wise direction from its OFF position to the ON position against the spring tension. The control arm is held in the ON position by the electromagnet E. The exciting coil of the hold-on electromagnet E is connected in series with the armature circuit. If the motor loses its load, current decreases and hence the strength of the electromagnet also decreases. The control arm returns to the OFF position due to the spring tension, Thus preventing the motor from over speeding. The starter also returns to the OFF position when the supply voltage decreases appreciably. L and F are the two points of the starte which are connected with the motor terminals.
ii) THREE POINT STARTER: (refer fig 2)

It is used for starting the shunt or compound motor. The coil of the hold on electromagnet E is connected in series with the shunt field coil. In the case of disconnection in the field circuit the control arm will return to its OFF position due to spring tension. This is necessary because the shunt motor will over speed if it loses excitation. The starter also returns to the OFF position in case of low voltage supply or complete failure of the supply. This protection is therefore called No Volt Release (NVR).

Over load protection:

When the motor is over loaded it draws a heavy current. This heavy current also flows through the exciting coil of the over load electromagnet (OLR). The electromagnet then pulls an iron piece upwards which short circuits the coils of the NVR coil. The hold on magnet gets de-energized and therefore the starter arm returns to the OFF position, thus protecting the motor against overload. L, A and F are the three terminals of the three point starter.

iii) FOUR POINT STARTER:

The connection diagram of the four point starter is shown in fig 3. In a four point starter arm touches the starting resistance, the current from the supply is divided into three paths. One through the starting resistance and the armature, one through the field circuit, and one through the NVR coil. A protective resistance is connected in series with the NVR coil. Since in a four point starter the NVR coil is independent of the field ckt connection, the d.c motor may over speed if there is a break in the field circuit. A D.C motor can be stopped by opening the main switch. The steps of the starting resistance are so designed that the armature current will remain within the certain limits and will not change the torque developed by the motor to a great extent.
Three Phase Transformer Connections

The primary and secondary windings of a transformer can be connected in different configurations as shown to meet practically any requirement. In the case of three phase transformer windings, three forms of connection are possible: “star” (wye), “delta” (mesh) and “interconnected-star” (zig-zag).

The combinations of the three windings may be with the primary delta-connected and the secondary star-connected, or star-delta, star-star or delta-delta, depending on the transformers use. When transformers are used to provide three or more phases they are generally referred to as a Polyphase Transformer.

Three Phase Transformer Star and Delta Configurations

But what do we mean by “star” and “delta” three-phase transformer connection. A three phase transformer has three sets of primary and secondary windings. Depending upon how these sets of windings are interconnected, determines whether the connection is a star or delta configuration. The available voltage which are each displaced from the other by 120 electrical degrees and flow of the transformers currents are also decided by the type of the electrical connection used on both the primary and secondary sides.

With three single-phase transformers connected together, the magnetic flux’s in the three transformers differ in phase by 120 time-degrees. With a single the three-phase transformer there are three magnetic flux’s in the core differing in time-phase by 120 degrees.

The standard method for marking three phase transformer windings is to label the three primary windings with capital (upper case) letters A, B and C, used to represent the three-phases of RED, YELLOW and BLUE. The secondary windings are labelled with small (lower case) letters a, b and c. Each winding has two ends normally labelled 1 and 2 so that, for example, the second winding of the primary has ends which will be labelled B1 and B2, while the third winding of the secondary will be labelled c1 and c2 as shown.
Transformer Star and Delta Configurations

Symbols are generally used on a three phase transformer to indicate the type or types of connections used with upper case Y for star connected, D for delta connected and Z for interconnected star primary windings, with lower case y, d and z for their respective secondaries. Then, Star-Star would be labelled Yy, Delta-Delta would be labelled Dd and interconnected star to interconnected star would be Zz for the same types of connected transformers.

Transformer Winding Identification

<table>
<thead>
<tr>
<th>Connection</th>
<th>Primary Winding</th>
<th>Secondary Winding</th>
</tr>
</thead>
<tbody>
<tr>
<td>Delta</td>
<td>D</td>
<td>d</td>
</tr>
<tr>
<td>Star</td>
<td>Y</td>
<td>y</td>
</tr>
<tr>
<td>Interconnected</td>
<td>Z</td>
<td>z</td>
</tr>
</tbody>
</table>

We now know that there are four ways in which three single-phase transformers may be connected together between primary and secondary three-phase circuits. The configurations are delta-delta, star-star, star-delta, and delta-star. Transformers for high voltage operation with the star connections has the advantage of reducing the voltage on an individual transformer, reducing the number of turns required and an increase in the size of the conductors, making the coil windings easier and cheaper to insulate than delta transformers.

The delta-delta connection nevertheless has one big advantage over the star-delta configuration, in that if one transformer of a group of three should become faulty or disabled, the two remaining ones will continue to deliver three-phase power with a capacity equal to approximately two thirds of the original output from the transformer unit.
Transformer Delta and Delta Connections

In a delta connected (Dd) group of transformers, the line voltage, \( V_L \) is equal to the supply voltage, \( V_L = V_S \). But the current in each phase winding is given as: \( 1/\sqrt{3} \times I_L \) of the line current, where \( I_L \) is the line current.

One disadvantage of delta connected three phase transformers is that each transformer must be wound for the full-line voltage, (in our example above 100V) and for 57.7 per cent, line current. The greater number of turns in the winding, together with the insulation between turns, necessitate a larger and more expensive coil than the star connection. Another disadvantage with delta connected three phase transformers is that there is no “neutral” or common connection.

In the star-star arrangement (Yy), (wye-wye), each transformer has one terminal connected to a common junction, or neutral point with the three remaining ends of the primary windings connected to the three-phase mains supply. The number of turns in a transformer winding for star connection is 57.7 per cent, of that required for delta connection.

The star connection requires the use of three transformers, and if any one transformer becomes fault or disabled, the whole group might become disabled. Nevertheless, the star connected three phase transformer is especially convenient and economical in electrical power distributing systems, in that a fourth wire may be connected as a neutral point, (n) of the three star connected secondaries as shown.
Transformer Star and Star Connections

The voltage between any line of the three-phase transformer is called the “line voltage”, \( V_L \), while the voltage between any line and the neutral point of a star connected transformer is called the “phase voltage”, \( V_P \). This phase voltage between the neutral point and any one of the line connections is \( \frac{1}{\sqrt{3}} \times V_L \) of the line voltage. Then above, the primary side phase voltage, \( V_P \) is given as.

\[
V_P = \frac{1}{\sqrt{3}} \times V_L = \frac{1}{\sqrt{3}} \times 100 = 57.7 \text{ Volts}
\]

Result:
STUDY OF INDUCTION MOTOR STARTERS

AUTO – TRANSFORMER STARTING

An auto transformer starter consists of an auto transformer and a switch as shown in the fig. When the switch S is put on START position, a reduced voltage is applied across the motor terminals. When the motor picks up speed, say to 80 per cent of its normal speed, the switch is put to RUN position. Then the auto-transformer is cut out of the circuit and full rated voltage gets applied across the motor terminals.

(Ref. To text book for fig)

The circuit dia in the fig is for a manual auto-transformer starter. This can be made push button operated automatic controlled starter so that the contacts switch over from start to run position as the motor speed picks up to 80% of its speed. Over-load protection relay has not been shown in the figure. The switch S is air-break type for small motors and oil break type for large motors. Auto transformer may have more than one tapping to enable the user select any suitable starting voltage depending upon the conditions.

Series resistors or reactors can be used to cause voltage drop in them and thereby allow low voltage to be applied across the motor terminals at starting. These are cut out of the circuit as the motor picks up speed.

STAR–DELTA METHOD OF STARTING:

The starter phase windings are first connected in star and full voltage is connected across its free terminals. As the motor picks up speed, the windings are disconnected through a switch and they are reconnected in delta across the supply terminals. The current drawn by the motor from the lines is reduced to as compared to the current it would have drawn if connected in delta. The motor windings, first in star and then in delta the line current drawn by the motor at starting is reduced to one third as compared to starting current with the windings delta-connected.

In making connections for star-delta starting, care should be taken such that sequence of supply connections to the winding terminals does not change while changing from star connection to delta connection. Otherwise the motor will start rotating in the opposite direction, when connections are changed from star to delta. Star-delta starters are available for manual operation using push button control. An automatic star – delta starter used time delay relays (T.D.R) through which star to delta connections take place automatically with some pre-fixed time delay. The delay time of the T.D.R is fixed keeping in view the starting time of the motor.

(Ref. To text book for fig)
FULL VOLTAGE OR DIRECT –ON-LINE STARTING

When full voltage is connected across the stator terminals of an induction motor, large current is drawn by the windings. This is because, at starting the induction motor behaves as a short circuited transformer with its secondary, i.e. the rotor separated from the primary, i.e. the stator by a small air-gap.

At starting when the rotor is at standstill, emf is induced in the rotor circuit exactly similar to the emf induced in the secondary winding of a transformer. This induced emf of the rotor will circulate a very large current through its windings. The primary will draw very large current from the supply mains to balance the rotor ampere-turns. To limit the stator and rotor currents at starting to a safe value, it may be necessary to reduce the stator supply voltage to a low value. If induction motors are started direct-on-line such a heavy starting current of short duration may not cause harm to the motor since the construction of induction motors are rugged. Other motors and equipment connected to the supply lines will receive reduced voltage. In industrial installations, however, if a number of large motors are started by this method, the voltage drop will be very high and may be really objectionable for the other types of loads connected to the system. The amount of voltage drop will not only be dependent on the size of the motor but also on factors like the capacity of the power supply system, the size and length of the line leading to the motors etc. Indian Electricity Rule restricts direct on line starting of 3 phase induction motors above 5 hp.

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